

BNAM 2008

Volume dependent impact sound insulation

Commonly use in the Nordic countries: $L'_{n,w}$

Weighted normalized impact sound pressure level

“Example from court” (2003 - 2005)

Situation

- **Old requirements** (project started before 1997)
 - $L'_{n,w} \leq 58$ dB
 - (this example is however still relevant)
- Structure*:
 - 200 mm concrete
 - 3 mm polyurethane foam
 - Parquet

*Today the minimum requirement is $L'_{n,w} \leq 58$ dB,
=> f.i. 250 mm concrete w/parquet on 5 mm foam

Intital measurements

- Acceptable values in small rooms
- Excessive values in larger room
- Detailed evaluations based on:
 - Vibration measurements*
 - Parquette on different sheets*
 - Calculations with BASTIAN

INDICATE STRONG VOLUME DEPENDENCE*

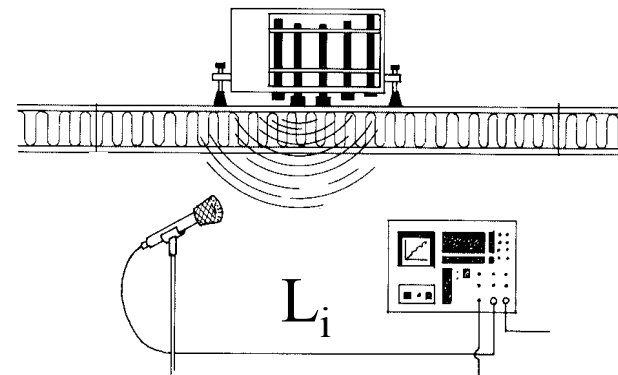
Bastian/EN 12354 shows less volume dependence with
"standard" input values.

WHY ANNOYANCE

- Impact sound is one of the most common reason for annoyance in dwellings.
- Expectations have changed (This case was brought to court several years after the 5 dB change in the regulations)
- NS 8175 indicates that 20 % can be annoyed even with the latest minimum requirements, Class C: $L'_{n,w} \leq 53$ dB

Field measurements

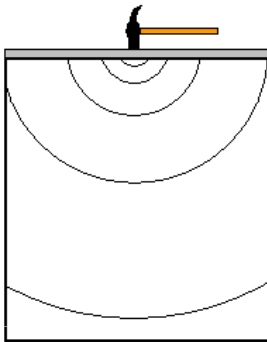
- $L'_n = L_i + 10 \lg(A/A_0)$
 - A = absorption area
 - $A_0 = 10 \text{ m}^2$
- Weighting:
 - $L'_{n,w}$ is found by use of a reference curve



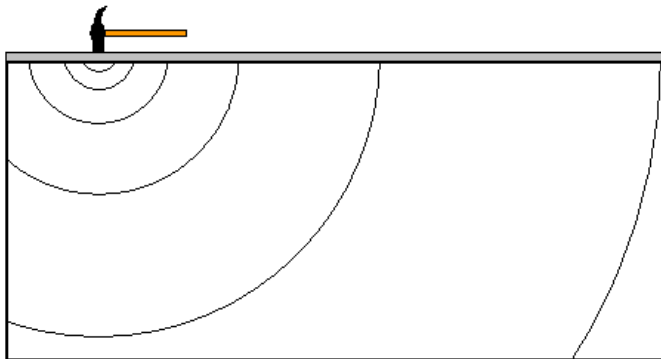
Requirements \Leftrightarrow measured

Situation	$L'_{n,w}$
Between rooms in flats 1987	≤ 58 dB
Between rooms in flats 1997 (2008)	≤ 53 dB
Living room to sitting room (typical)	60 dB
Sleeping room to sleeping room (typical)	54 dB

Expected sound energy distribution

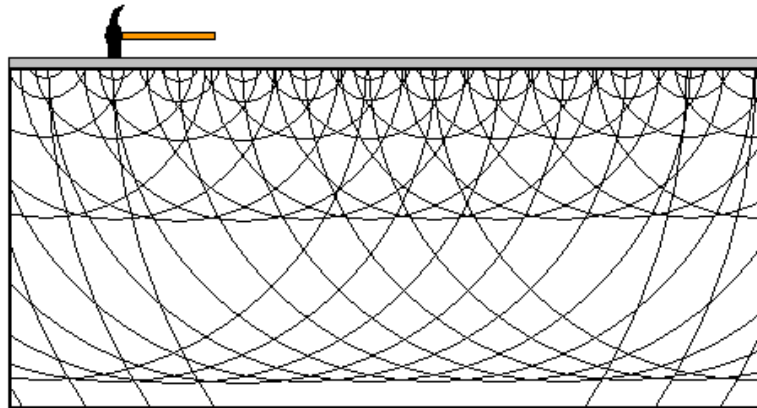
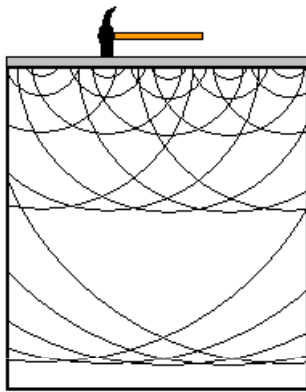


- **Light weight floor** structures tends to be local reacting.



- Thus the sound level is **reduced** with increasing room volume.

Expected sound energy distribution



- Heavy floor structures as **concrete slabs** tends to spread energy due to the structural reverberation
- Thus the sound level is **less dependant** on the room size.

Consequence of "Normalization"

1. Definition: $L'_n = L_i + 10 \lg(A/A_0)$
 2. $A = 0,161 V / T$
 - V = Volume of receiving room
 - T = Reverberation time in receiving room
 3. Inserting (2) in to (1) gives:
 - $L'_n = L_i + 10 \lg V - 10 \lg T - K$
 - Where $K = 10 \lg(A_0/0,161) = 18 \text{ dB}$
- The normalized impact sound pressure level L'_n increases with the volume V , if the sound level L_i , and the reverberation time T , is unchanged.

Realities in this case?

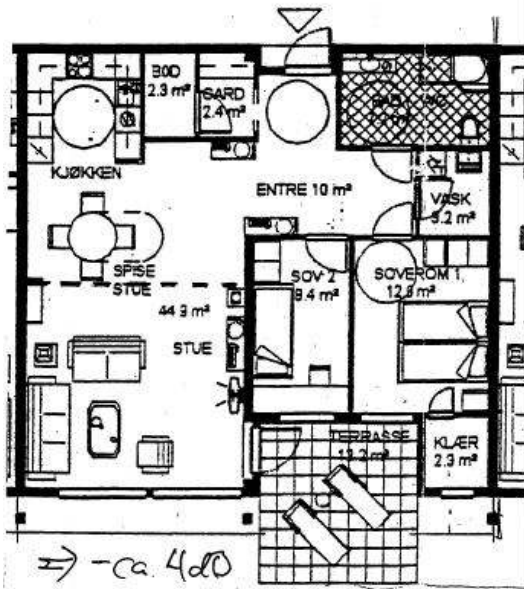
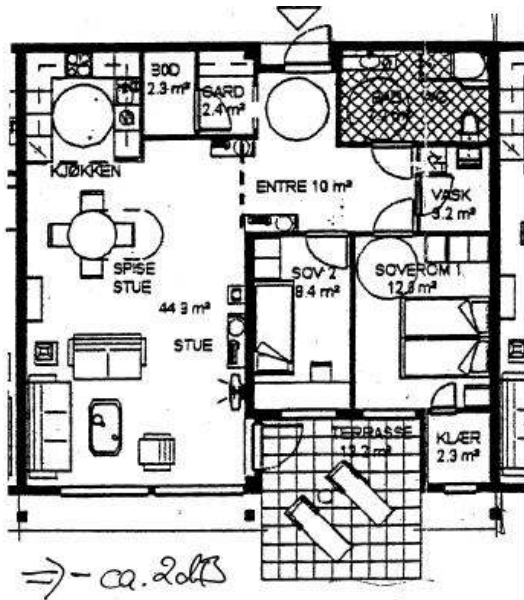
- Expectively acceptable solution.
- No "mistakes" revealed in the workmanship.
- "Unpredictable" effect of large volumes.
- Sweden had included volume limitations in their requirements at this time.
- Norway started such discussions at the beginning of these measurements.

Relevant changes in regulations

- Sweden introduced a volume limitation of 31 m³ in feb. 04, together with a restriction of 2 dB => "flat" limit above 50 m³
- Norway introduced a volume limit of 100 m³ in april 05.
- Standardized impact sound pressure level is discussed in other countries:
 - e.g: $L'_n = L_i + 10 \lg(T/T_o)$
- Both alternatives leads to "Volume independence" at least for larger volumes

This case: Large and complex volumes

- The first measurements were made by Stavanger Technical School. They decided to use the complete volume.
- The ISO standard allows to close off parts of the room when the situation is complex.
- Limitations as shown with dotted lines could have given -2 dB (top) or -4 dB (bottom)



Results

- Impact sound pressure levels – various methods:

Room	$L_{p,A}$	$L'_{n,w}$	$L'_{n,w}$ ($<100\text{m}^3$)	$L'_{n,w}$ ($<31\text{m}^3$)	$L'_{n,T,w}$
Living room	61 dBA	60 dBA	58-59 dB	53 dB	53 dB
Sleeping room	61 dBA	54 dBA	54 dB	54 dB	55 dB

$L_{p,A}$ is the measured sound pressure level – directly without weighting

Similar examples

Eks	Bygn.type	LA	V	L'n,w	Krav NO	Overskridelse	L'n,w når V=31m3	Møblert?
1,1	Kontor	64,8	344	66	63	3 dB	55	Ja
1,2	Kontor	64,9	32	55	63	-	55	Ja
2,1	Bolig (-87)	63,1	86	56	58	-	51	Nei
2,2	Bolig (-87)	59,4	53	53	58	-	51	Ja
3,1	Bolig (-97)	60,3	85	53	53	0	49	Nei
3,2	Bolig (-97)	59,4	58	52	53	-	49	Nei
3,3	Bolig (-97)	61,2	26	49	53	-	50	Nei
							L'n,w når V<31m3	
4,1	Bolig (87)	60,7	138	60	58	2	53	Ja
4,2	Bolig (87)	60,9	26	54	58	-	54	Ja
5,1	Bolig (97)	41,3	17	37	53	-	37	Ja
5,2	Bolig (97)	47,1	102	46	53	-	41	Ja
6,1	Bolig (97)	58,5	35	48	53	-	48	Lite (nei?)
6,2	Bolig (97)	57,5	110	52	53	-	47	Lite (nei?)
7,1	Bolig (97)	73,8	7	61	53?	8	61	Ja
7,2	Bolig (97)	70,1	22	63	53?	10	63	Ja
7,3	Bolig (97)	68,6	83	66	53?	13	61	Ja
8,1	Bolig (97)	52,0	27	51	53	-	51	Nei?
8,2	Bolig (97)	51,4	87	53	53	-	48	Nei?
* Merk: I resultatene fra 4,1 til 8,2 er det bare korrigeret for romvolumer som er større enn 31 m3								

Our technical conclusion for this "CASE"

- Recognized acceptable solutions are used
- Good workmanship is performed
- $L'_{n,w}$ in small rooms are well within limits
- $L'_{n,w}$ in large rooms exceeds requirements
mainly due to the definition of the term.

Juridical Decision

The impact sound pressure level
must be reduced
in the large rooms
to fulfill the requirements to

$$L'_{n,w}$$

Questions

- Is it possible that higher annoyance is claimed in the large rooms than in the small (even if the actual sound pressure level is accepted to be similar)?
- Does the court understand the "weak part" better than technical explanations?

TECHNICAL CONCLUSION

- $L'_{n,w}$ increases significantly with V
- With no volume limitations, ΔL must be better / higher in larger rooms
- Even with a volume limit of 100 m^3 (as in Norway), it is relevant to distinguish between solutions in small and large rooms.